Moisture-dependent physical properties of wheat

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A b s t r a c t. The various physical properties of five varieties of wheat were evaluated for moisture content in the range of 0 to 22% d.b. The average length, width, thickness and thousand-kernels weight were 7.08, 3.27, 2.98 mm and 29.6 g at a moisture content of 7.4% d.b. The average length for dry land farming wheat varieties was longer than for that irrigated. The average geometric mean diameter and percentage of sphericity was 4.26 and 60. Studies on rewetted wheat showed that the bulk and true densities decreased from 740 to 538.8 kg m⁻³ and 1240 to 847.2 kg m⁻³, whereas the corresponding bulk porosity increased. The static coefficient of friction varied from 0.279 to 0.450 over different material surfaces, while the dynamic angle of repose varied from 34.7 to 45° within the moisture range studied.

K e y w o r d s: physical properties, wheat, moisture content

INTRODUCTION

In Iran, wheat is cultivated on $6.567 \cdot 10^{10} \text{ m}^2$ with an annual production of $11.227 \cdot 10^9$ kg (Ministry of Jihad - e - Agriculture, 2000). To design a machine for handling, cleaning, conveying, storing and milling, the physical properties of wheat at different moisture contents must be known.

The thousand-kernels weight (TKW), angle of repose and static coefficient of friction of faba beans increased with an increase in moisture content while bulk density decreased (Fraser *et al.*, 1978). Chung and Converse (1971) reported that in the bulk density of rewetted wheat, up to 30% of the moisture content decreased but for a higher moisture content it will increase. The lentil seed dimensions, bulk density, porosity, projected area, terminal velocity, static and dynamic coefficients of friction were evaluated in the moisture range of 6.5 to 32.65% by Carman (1996). Gupta and Prakash (1990) determined the physical properties of the chickpea and the green gram in the moisture content range of 7.5 to 31.6% d.b. and reported that the TKW and mean diameter increased but the bulk density decreased with an increase in moisture content. Dutta *et al.* (1988) de termined the various properties of the chickpea including shape, TKW, sphericity, roundness, size, volume, surface area, bulk density, true density, porosity, static coefficient of friction and angle of repose in the moisture range of 9.64 to 31.0% d.b.

A review of the literature has revealed that detailed measurements of the principal dimensions and the variation of physical properties of wheat at various levels of moisture content have not been investigated. The object of this study was to investigate some moisture-dependent physical properties, namely, linear dimensions, size, sphericity, TKW, bulk density, true density, static and dynamic angle of repose and the static coefficient of friction of irrigated and dry land wheat varieties.

MATERIALS AND METHODS

In this study, three varieties of irrigated wheat, Falat, Ghods, and Mahdavi, and two varieties of dry land wheat, Sardari and Cross Alborz, were selected from popular varieties in Iran to determine their moisture-dependent physical properties. The samples were kept in plastic bags at the initial moisture content of around 8%. The grain was cleaned manually to remove foreign matter and any damaged or immature grain. All the physical properties of the grain were assessed at moisture levels of 0 to 22% d.b. at 8 levels of moistures (0, 5, 8, 10, 12, 14, 18, 22%) for each moisture content 5 replications. In order to achieve the desired moisture content for drying, a pre-determined time and temperature table for the grain was followed; the grain was placed in an oven to reach the proper moisture content. For rewetting: a certain amount of pure water was added to the sample using the following Eq. (1) and placed in a refrigerator for 104 h to reach to the proper moisture content.

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$$Wa = Wi (Mi - Mf) / 100 - Mi, \qquad (1)$$

where: Wa – mass of water added, Wi – initial sample mass, Mi – initial moisture content, Mf – desired (final) moisture content.

The sample was then weighed and placed in an oven for 22 h to determine the moisture content on a dry basis.

The moisture content of the whole grain was determined by drying it in an oven at $130 \pm 2^{\circ}$ C for different times and temperature tables followed by cooling in desiccators before finally weighing it.

To determine the average size of the grain at 7.3% moisture content, a sample of 50 randomly selected kernels of each variety and their three principal dimensions were measured using a venire calliper to an accuracy of 0.01 mm. The geometric mean diameter, D_{gm} , of the grain was calculated by using the following relationship:

$$D_{gm} = (LDT)^{1/3},$$
 (2)

where *L*, *D*, *T* is the length, width, and thickness (mm) of the kernel, respectively. Mohsenin (1986) expressed the degree of sphericity as follows:

$$\phi = (LDT)^{1/3} / L. \tag{3}$$

The TKW was determined by the standard method using a numerical seed counter, the Elehemel model of the Hemstead Company, to count them; it was then weighed. The bulk density of the grain based on volume occupied by the bulk sample was measured by placing a sample with a pre-determined moisture content into a known volume of 20 cc Becker. The bulk density was determined by dividing this weight by the 20 cc volume. This method was repeated five times; the averaged bulk density was thus determined. True density – defined as the ratio of the volume of particles – was determined using the water displacement method to the known volume of the sample. The porosity of the bulk is the ratio of the volume of the internal pores within the kernels to its bulk volume and was determined as Eq. (4):

$$\varepsilon = 100 \Big[1 - \left(\rho_d / \rho_t \right) \Big], \tag{4}$$

where: ε – the porosity (%), ρ_d – the bulk density (kg m⁻³), and ρ_t – the true density (kg m⁻³).

For measuring the static and dynamic angle of repose, the apparatus (Fig. 1) consisted of a plywood box of 140 mm by 160 mm by 35 mm and two plates: fixed and adjustable. The grain was dropped into the box from a height of 20 cm until full and was then levelled. The adjustable plate was then inclined gradually (Fig. 1) until the kernel start to move at that angle; the filling angle or the static angle of repose was then read off from a graduated scale. The plate was then moved upward till the whole grain mass started to move; this was the read off the graduated scale. The static coefficient of friction μ was determined for five different structural materials, namely, plywood, glass, compressed plastic, galvanized iron and stainless steel sheeting. An aluminium cylinder of 75 mm diameter and 50 mm height was placed on an adjustable tilting plate (Fig. 2), faced with the test surface and filled with about 150 g of the sample. The cylinder was raised slightly so as not to touch the surface. The structural surface with the cylinder resting on it was inclined gradually until the box just started to slide down. The angle of tilt was read from the graduated scale (Dutta *et al.*, 1988; Fraser *et al.*, 1978; Shepherd and Bhardwaj, 1986). All the above experiments were replicated five times, unless stated otherwise and the average values reported.



Fig. 1. Angle of repose (filling and emptying) apparatus.



Fig. 2. Static coefficient of friction.

RESULTS AND DISCUSSIONS

Seed dimensions

Table 1 shows the mean and standard deviations of 50 measurements of the dimensions of each wheat variety with a moisture content of 7.4%. The results show a coefficient of variation of 5.64% of the mean dimensions. It also indicated that the length of the Sardari and Cross Alborz are the longest – 7.36 and to 7.31 mm, respectively. The Mahdavei and Cross Alborz varieties had the highest sphericity and mean of geometric mean diameter. Wheat varieties for dry land were longer and thinner than for irrigated land. The mean percentage of sphericity for wheat was 60.2%.

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T a ble 1. Means and standard deviation of wheat varieties dimensions, geometric mean diameters and percentage sphericity at 7.4% moisture content

Variety	Length	Width Thickness		Geometric mean diameter	Sphericity (%)
Falat	6.96 ± 0.42	3.62±0.30	3.27±0.30	4.35 ± 0.26	62
Ghods	6.64 ± 0.41	3.43 ± 0.24	3.07 ± 0.28	4.11±0.25	62
Mahdavei	7.15 ± 0.41	3.95 ± 0.27	3.61 ± 0.19	4.67 ± 0.22	65
Cross Alborz	7.31 ± 0.56	2.85 ± 0.25	2.56 ± 0.21	4.65 ± 0.22	64
Saradari	7.36 ± 0.43	2.51 ± 0.17	2.37 ± 0.17	3.52 ± 0.18	48
Mean	7.08 (CV=6%)	3.27	2.98	4.26	60

CV - coefficient of variation.

The thousand-kernels weight (TKW)

The TKW W_t increased linearly from 23.2 g to 39.7 g (probability < 0.01) when the moisture content increased from 0 to 22 % d.b. as shown in Fig. 3. The relationship between the TKW and the moisture content can be represented as:

$$W_t = 22.6 + 0.79 M \tag{5}$$

with a value for \mathbb{R}^2 of 0.96. The average TKW at 7.4 % moisture content was 29.6 g with 4.6 g standard deviation. Wheat has a small grain size, compared with other commonly grown crops; for example at a moisture content of 13.15% d.b., the TKW for wheat is 34.6 g while it is 30.15 g for the green gram (Nimkar and Chattopadyay, 2001), 75 g for the pigeon pea (Shephered and Bhardwaj, 1986), 117 g for the soya bean (Kulkarni *et al.*, 1993), 176 g for the chickpea (Dutta *et al.*, 1988), and 120 g for the faba bean (Fraser *et al.*, 1978).

Bulk density

Bulk density at different moisture levels varied from 740 to 538.8 kg m⁻³ and indicated a decrease in bulk density with an increase in moisture content with significant (probability < 0.01) variations as shown in Fig. 4. This is due to the fact that an increase in mass owing to moisture gain in the grain sample was lower than the accompanying volumetric expansion of the bulk. The grain bulk density was found to bear the following relationship with moisture content:

$$\rho_d = 754.3 - 10.4 \, M \tag{6}$$

with a value for R^2 of 0.96. The negative linear relationship of bulk density with moisture content was also observed by various other research works (Carman, 1996; Dutta *et al.*, 1988; Gupta and Prakash, 1990; Shephered and Bhardwaj, 1986). Mohsenin (1986) has shown that bulk density at 11.9% moisture content for wheat was higher, 767 kg m⁻³, than the value found in this study (645 kg m⁻³).

True density

The true density of the wheat was measured at different moisture levels and was found to be negatively correlated and varied from 1240 to 847.2 kg m⁻³ (Fig. 5). The variation in true density with the moisture content was significant



Fig. 3. Effect of moisture content on the TKW.



Fig. 4. Effect of moisture content on bulk density.



Fig. 5. Effect of moisture content on true density.

(probability < 0.01). The decrease in true density values with the increase in moisture content might be attributable to the relatively higher true volume as compared to the corresponding mass of the grain attained due to the adsorption of water. The results were in conformity with those of other researchers: (Deshpande *et al.*, 1993; Dutta *et al.*, 1988; Shephered and Bhardwaj, 1986). A regression equation with the best fit to the data was as follow:

$$\rho_t = 1258.2 - 18.64 \, M \tag{7}$$



Fig. 6. True and bulk density relationship at different moisture levels.

with a value for R^2 of 0.95. The average value for true density of winter wheat was reported (Nelson, 1980), as 1340 kg m⁻³ at 11.4% moisture content higher than the value found in this study, 1010 kg m⁻³. However, there is a strong correlation between bulk density and true density (Fig. 6) which increases linearly as shown by others (Chung and Converse, 1971; Nelson, 1980).

There was a variation from 32.6 to 37.4% for the porosity at the moisture levels.

Angle of repose

The experimental results for the dynamic angle of repose with respect to moisture content are shown in Fig. 7. The values were found to increase from 34.7 to 45° in the moisture range of 0 to 22% d.b. The values for wheat are higher than those for the green gram (Nimkar and Chattopadyay, 2001), the faba bean (Fraser *et al.*, 1978), and the pigeon pea (Sphered and Bhardwaj, 1986). The static angle of repose for wheat has the following relationship with its moisture content:

$$\theta_s = 28.6 + 0.37 M$$
 (8)

with a value for R^2 of 0.80.



Fig. 7. Effect of moisture content on dynamic angle of repose.

T :	a b	l e	2.	Static	coefficient	of	friction	for	wheat	varieties
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Moisture content (% d.b.)	Coefficient of friction (°)							
_	Plywood	Glass	Compressed plastic	Galvanized iron	Stainless steel			
0	0.367	0.279	0.300	0.335	0.317			
5.5	0.366	0.288	0.297	0.340	0.336			
8	0.375	0.293	0.297	0.340	0.323			
10	0.384	0.305	0.323	0.349	0.330			
12	0.389	0.314	0.326	0.358	0.340			
14	0.398	0.332	0.361	0.363	0.349			
18	0.422	0.367	0.401	0.393	0.367			
22	0.450	0.401	0.433	0.415	0.398			

The static coefficients of friction for wheat, determined with respect to five different structural surfaces, are listed in Table 2. It is observed that the static coefficient of friction of wheat increased with the increase in the moisture content on all surfaces. At all moisture contents, the static coefficient of friction was greatest against plywood (0.367–0.450) followed by compressed plastic (0.30–0.433), galvanized iron (0.335–0.415), glass (0.279–0.401), and the least for stainless-steel sheeting (0.317–0.398). It was observed that moisture had more effect than did the material's surface on the static coefficient of friction due to the increase of adhesion at higher moisture values.

CONCLUSIONS

1. At a moisture content of 7.4% d.b., the average length, width, thickness of wheat grain was 7.08, 3.27, and 2.98 mm, respectively. The dry land wheat varieties were longer and thinner than the variety originating from irrigated land. The average TKW was 29.6 g. The average geometric mean diameter and percentage sphericity was 4.26 and 60.

2. The bulk and true densities decreased from 740 to 538.8 kg m⁻³ and 1240 to 847.2 kg m⁻³, whereas the corresponding bulk porosity increased at a moisture content of 0 to 22%. True and bulk densities were lower for the Iranian wheat varieties than for those reported.

3. The dynamic angle of repose varied from 34.7 to 45° and the static coefficient of friction varied from 0.279 to 0.450 over different material surfaces in the specified moisture content.

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